

Show work – except for ♣ fill-in-blanks-problems.

Constraints (e.g., contact, rolling, and closed-chains/linkages)

10.1 ♣ Velocity variables and degrees of freedom (Section 11.1).

Determine the minimum number of unknown *velocity variables* necessary to characterize the motion of the following systems in a reference frame N . Regard Q as a free-flying particle and A as a rigid body that is **free** to translate and rotate in 3D-space. Choose and **define** velocity variables that suffice to describe the motion (Note: The choice of velocity variables is **not unique**).

Optional: **Sketch** each system with names for each point/body.

System (Q , B , or A and B)	Degrees of freedom	Choice of velocity variables
Free-flying particle Q .	3	v_x v_y v_z ${}^N\vec{v}^Q = v_x \hat{n}_x + v_y \hat{n}_y + v_z \hat{n}_z$
Particle Q moving in a slot (slot is parallel to a unit vector \hat{n}).	1	v ${}^N\vec{v}^Q = v \hat{n}$
Free-flying rigid body B .	6	ω_x ω_y ω_z v_x v_y v_z ${}^N\vec{\omega}^B = \omega_x \hat{b}_x + \omega_y \hat{b}_y + \omega_z \hat{b}_z$ ${}^N\vec{v}^{B_o} = v_x \hat{n}_x + v_y \hat{n}_y + v_z \hat{n}_z$
Rigid body B connected to rigid body A by a revolute joint. (A connects to B at point A_B of A)	7	ω_x ω_y ω_z v_x v_y v_z ω_B ${}^N\vec{\omega}^A = \omega_x \hat{a}_x + \omega_y \hat{a}_y + \omega_z \hat{a}_z$ ${}^N\vec{v}^{A_B} = v_x \hat{a}_x + v_y \hat{a}_y + v_z \hat{a}_z$ ${}^A\vec{\omega}^B = \omega_B \hat{\lambda}$
Rigid body B connected to rigid body A by a rigid joint.	6	ω_x ω_y ω_z v_x v_y v_z ${}^N\vec{\omega}^A = \omega_x \hat{a}_x + \omega_y \hat{a}_y + \omega_z \hat{a}_z$ ${}^N\vec{v}^{A_B} = v_x \hat{n}_x + v_y \hat{n}_y + v_z \hat{n}_z$
Rigid body B connected to A by a ball-and-socket joint.	9	ω_x ω_y ω_z v_x v_y v_z ω_x^B ω_y^B ω_z^B ${}^N\vec{\omega}^A = \omega_x \hat{a}_x + \omega_y \hat{a}_y + \omega_z \hat{a}_z$ ${}^N\vec{v}^{A_B} = v_x \hat{a}_x + v_y \hat{a}_y + v_z \hat{a}_z$ ${}^A\vec{\omega}^B = \omega_x^B \hat{b}_x + \omega_y^B \hat{b}_y + \omega_z^B \hat{b}_z$
Rigid body B connected to A by a revolute angular velocity motor. (A revolute angular velocity motor <u>specifies</u> B 's angular velocity in A)	6	ω_x ω_y ω_z v_x v_y v_z ${}^N\vec{\omega}^A = \omega_x \hat{a}_x + \omega_y \hat{a}_y + \omega_z \hat{a}_z$ ${}^N\vec{v}^{A_B} = v_x \hat{n}_x + v_y \hat{n}_y + v_z \hat{n}_z$
Rectangular box B sliding on a flat rigid surface fixed in N . (B contacts N at a single vertex B_o of B)	5	ω_x ω_y ω_z v_x v_y ${}^N\vec{v}^{B_o} = v_x \hat{n}_x + v_y \hat{n}_y$ ${}^N\vec{\omega}^B = \omega_x \hat{b}_x + \omega_y \hat{b}_y + \omega_z \hat{b}_z$
Rectangular box B sliding on a flat rigid surface fixed in N . (B contacts N on a single edge of B)	4	ω_y ω_z v_x v_y ${}^N\vec{v}^{B_o} = v_x \hat{n}_x + v_y \hat{n}_y$ ${}^N\vec{\omega}^B = \omega_y \hat{b}_y + \omega_z \hat{b}_z$
Rectangular box B sliding on a flat rigid surface fixed in N . (B contacts N on one surface of B)	3	ω_z v_x v_y ${}^N\vec{v}^{B_o} = v_x \hat{n}_x + v_y \hat{n}_y$ ${}^N\vec{\omega}^B = \omega_z \hat{b}_z$

10.2 Velocity and acceleration of a wheel sliding on a plane (Section 11.12).

The following shows a wheel B of radius R in contact with a horizontal road N .

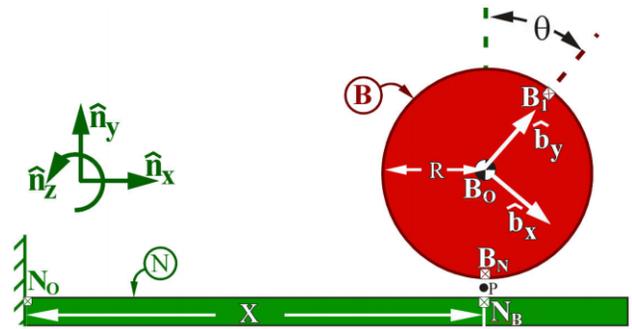
Point N_o is fixed on N .

Point B_o is the wheel's geometric center.

Point B_1 is fixed to B at the wheel's periphery.

Right-handed orthogonal unit vectors $\hat{n}_x, \hat{n}_y, \hat{n}_z$ and $\hat{b}_x, \hat{b}_y, \hat{b}_z$ are fixed in N and B , with

- \hat{n}_x horizontally-right
- \hat{n}_y vertically-upward
- $\hat{n}_z = \hat{b}_z$ parallel to B 's angular velocity in N
- \hat{b}_y directed from B_o to B_1



B 's translation in N is characterized by x , the \hat{n}_x measure of B_o 's position from N_o .

B 's rotation in N is characterized by θ , the angle from \hat{n}_y to \hat{b}_y with $-\hat{n}_z$ sense.

Succinctly answer each question in terms of $R, x, \dot{x}, \ddot{x}, \theta, \dot{\theta}, \ddot{\theta}, \hat{n}_x, \hat{n}_y, \hat{n}_z, \hat{b}_x, \hat{b}_y, \hat{b}_z$.

- (a) Determine B 's angular velocity in N and B 's angular acceleration in N .

Use **definitions** to calculate B_o 's velocity in N and B_1 's velocity in N .

Result:

$${}^N\vec{\omega}^B = -\dot{\theta}\hat{n}_z \quad {}^N\vec{\alpha}^B = -\ddot{\theta}\hat{n}_z \quad {}^N\vec{v}^{B_o} = \dot{x}\hat{n}_x \quad {}^N\vec{v}^{B_1} = \dot{x}\hat{n}_x + R\dot{\theta}\hat{b}_x$$

- (b) Find B_1 's velocity in N at the **instant** when B_1 is in contact with N .

Result: (in terms of $\hat{n}_x, \hat{n}_y, \hat{n}_z$) ${}^N\vec{v}^{B_1}\Big|_{\text{contact}} = (\dot{x} - R\dot{\theta})\hat{n}_x$

- (c) Point B_N designates the point **of** B that is in contact with N at each **instant**.

Provide a formula relating ${}^N\vec{v}^{B_N}$ to ${}^N\vec{v}^{B_o}$ [this formula should not contain a derivative and uses the fact that B_o and B_N are both points **of** (fixed on) B]. Then, express ${}^N\vec{v}^{B_N}$ in terms of $R, \dot{x}, \dot{\theta}$.

Similarly, provide a derivative-free formula relating ${}^N\vec{a}^{B_N}$ to ${}^N\vec{a}^{B_o}$ and then calculate ${}^N\vec{a}^{B_N}$.

Result:

$${}^N\vec{v}^{B_N} = {}^N\vec{v}^{B_o} + {}^N\vec{\omega}^B \times \vec{r}^{B_N/B_o} = (\dot{x} - R\dot{\theta})\hat{n}_x \quad (10.3)$$

$${}^N\vec{a}^{B_N} = {}^N\vec{a}^{B_o} + {}^N\vec{\alpha}^B \times \vec{r}^{B_N/B_o} + {}^N\vec{\omega}^B \times ({}^N\vec{\omega}^B \times \vec{r}^{B_N/B_o}) = (\ddot{x} - R\ddot{\theta})\hat{n}_x + \dot{\theta}^2 R\hat{n}_y \quad (10.4)$$

- (d) Point B_N 's position vector from N_o is **always** $\vec{r}^{B_N/N_o} = x\hat{n}_x$.

Why is your previous result for ${}^N\vec{v}^{B_N}$ **not** the time-derivative in N of \vec{r}^{B_N/N_o} ?

Why is your previous result for ${}^N\vec{a}^{B_N}$ **not** the time-derivative in N of ${}^N\vec{v}^{B_N}$?

$${}^N\vec{v}^{B_N} = (\dot{x} - R\dot{\theta})\hat{n}_x \neq \frac{N_d}{dt}\vec{r}^{B_N/N_o}$$

$${}^N\vec{a}^{B_N} = (\ddot{x} - R\ddot{\theta})\hat{n}_x + \dot{\theta}^2 R\hat{n}_y \neq \frac{N_d}{dt}{}^N\vec{v}^{B_N}$$

Explain:

Point B_N is the point **of** B in contact with N . Point B_1 is only B_N for an **instant**.

The time-derivative of B_1 's position vector at this **instant** **does not** produce its velocity!

If B maintains contact with N , point B_N is continuously being **renamed** – which is strange, but useful.

- (e)
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|---|--------------------|
| • The symbols B_N and B_1 sometimes designate the same point. | True /False |
| • Point B_1 is always the name of the same (one) specific point of B . | True /False |
| • Point B_N is always the name of the same (one) specific point of B . | True/ False |
| • Point B_N is continuously renamed as B rotates in N . | True /False |
| • When B_1 is in contact with N , ${}^N\vec{v}^{B_1}\Big _{\text{contact}}$ has the same meaning as ${}^N\vec{v}^{B_N}$. | True /False |