F = ma

20.5 MG road-maps for efficient statics and dynamics

A modern way to efficiently form static or dynamic equations with FBDs is to:¹

- Choose *scalar variables* that describe the relevant *unknown* configuration, motion, or forces.
- Complete the associated *MG road-maps* and *free-body diagrams*.²
- Complete the calculations specified by the *MG road-map equation*.

Variable	Translate/ Rotate	Direction (unit vector)	$\stackrel{\mathrm{System}}{S}$	$_{\rm of }^{\rm FBD}$	About point	MG road-map equation	Additional Unknowns	
				Draw			?	
* If applicable: Additional <i>constraint equations</i> and their time-derivatives (e.g., closed linkages or rolling).								

MG road-map for efficient statics and dynamics.

Column	Enter the following information						
$\begin{array}{c}1\\2\\3\end{array}$	Unknown scalar variable (e.g., a position, velocity, force, or torque variable). Type of motion associated with the variable: translate or rotate . Vector direction (e.g., unit vector $\hat{\mathbf{u}}$) associated with the direction of motion.						
4	List of objects whose motion (e.g., velocity or angular velocity) is directly effected by the variable in column 1 ("freeze" any variable other than the variable in column 1 and decide what objects must move). This picks a system S that reduces/eliminates constraint forces. Note: If the variable in column 1 is a force measure, treat it as a velocity measure and determine what objects move. If it is a torque measure, treat it as an angular velocity measure and determine what objects move.						
5	<u>Draw</u> a <i>free-body diagram</i> of system S (<u>draw</u> relevant contact/distance forces). Note: See force/torque models for gravity, springs, dampers, air-resistance, etc., in Chapter 19.						
6	If column 2 was rotate , choose a point O (or line L) about which moments are to be taken. Note: Choose point O to eliminate moments of unknown forces (e.g., contact forces on S) – look at FBD. Note: To facilitate calculations, you can slide the "about point" along the line L parallel to $\hat{\mathbf{u}}$. This is because $\hat{\mathbf{u}} \cdot \vec{\mathbf{M}}^{S/O} = \hat{\mathbf{u}} \cdot \vec{\mathbf{M}}^{S/P}$ if both points O and P are on line L (proved in Section 17.1.3).						
7a	If column 2 was <u>translate</u> , use: (<i>N</i> is a Newtonian reference frame) $\hat{\mathbf{u}} \cdot (\vec{\mathbf{F}}_{\text{Dynamics}}^{S} = m^{S} * \vec{\mathbf{a}}_{\text{Scm}}^{S})$ or $\hat{\mathbf{u}} \cdot \vec{\mathbf{F}}_{\text{Statics}}^{S} = 0$						
10	To calculate $m^{S} * {}^{N}\vec{\mathbf{a}}^{S_{cm}}$ for a system S of objects A, B, C: $m^{S} * {}^{N}\vec{\mathbf{a}}^{S_{cm}} = m^{A} * {}^{N}\vec{\mathbf{a}}^{A_{cm}} + m^{B} * {}^{N}\vec{\mathbf{a}}^{B_{cm}} + m^{C} * {}^{N}\vec{\mathbf{a}}^{C_{cm}}$						
	If column 2 was <u>rotate</u> , use: $\hat{\mathbf{u}} \cdot (\vec{\mathbf{M}}_{(20.4)}^{S/O} = \frac{{}^{N}d {}^{N}\vec{\mathbf{H}}^{S/O}}{dt} + \dots)$ or $\hat{\mathbf{u}} \cdot \vec{\mathbf{M}}_{\mathbf{Statics}}^{S/O} = 0$						
7b	For a system S with a par- ticle Q and rigid body B: $\vec{H}^{S/O} = \vec{H}^{Q/O} + \vec{H}^{B/O}$ For rigid body B $\vec{H}^{B/O} = \vec{H}^{Q/O} \times m^{Q} \vec{v}^{Q}$ For rigid body B $\vec{H}^{B/O} = \vec{H}^{B/B_{p}} + \vec{r}^{B_{p}/O} \times m^{B} \vec{v}^{B_{cm}}$ where: $\vec{H}^{B/B_{p}} = \vec{I} \cdot \vec{v}^{B/B_{p}} + \vec{r}^{B_{cm}/B_{p}} \times m^{B} \vec{v}^{B_{p}}$						
8*	Additional constraint force/torque variables may appear in MG road-maps. If applicable, append configuration or motion <i>constraints</i> (e.g., closed linkages or rolling) that interrelate Column 1 position/velocity variables.						

See MG road-map examples in next sections and at <u>www.MotionGenesis.com</u> \Rightarrow <u>Textbooks</u> \Rightarrow <u>Resources</u>.

¹Mitiguy and Fregly invented MG road-maps to efficiently form static and dynamic equations. MG road-maps combine the simplicity of a spreadsheet with the physical insights of free-body diagrams. MG road-maps were inspired by the cleverness of D'Alembert and the mathematical rigor of Kane and Euler/Lagrange. MG road-maps are easy to teach/learn and approximate the efficiency of Kane's method for most systems (except embedded constraints like rolling/gears).

²*Free-body diagrams (FBDs)* are a means to an end, not an end in itself. *MG road-maps* help determine which FBDs to draw and what to do with them, – which differs significantly from knowing how to draw FBDs.

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120

Chapter 20: Dynamics: Laws of motion

20.5.1MG road-map: Projectile motion (2D)

A baseball (particle Q) flies over Earth N (a Newtonian reference frame). Aerodynamic forces on the baseball are modeled as $-b \vec{\mathbf{v}}$ ($\vec{\mathbf{v}}$ is Q's velocity in N). $\widehat{\mathbf{n}}_{x}$ is horizontally-right, $\widehat{\mathbf{n}}_{y}$ is vertically-upward, and N_{o} is home-plate (point fixed in N).

MG road-map for projectile motion x and y ($\hat{\mathbf{n}}_x, \hat{\mathbf{n}}_y$ measures of Q's position vector from N_0)

Variable	Translate/ Rotate	Direction (unit vector)	System S	$_{\mathrm{of}\ S}^{\mathrm{FBD}}$	About point	MG road-map equation
x				Draw	Not applicable	$\cdot \left(= \right)$
y				Draw	Not applicable	$\cdot \left(\begin{array}{c} = \\ (20.1) \end{array} \right)$

Solution and simulation link at <u>www.MotionGenesis.com</u> \Rightarrow <u>Textbooks</u> \Rightarrow <u>Resources</u>.

20.5.2MG road-map: Rigid body pendulum (2D)

A non-uniform density rigid rod A is attached at point A_0 of A by a frictionless revolute/pin joint to Earth N (Newtonian reference frame). The rod swings with a "pendulum angle" θ in a vertical plane that is perpendicular to unit vector $\hat{\mathbf{a}}_{z}$.

Variable	Translate/ Rotate	Direction (unit vector)	System	$\begin{array}{c} \text{FBD} \\ \text{of } S \end{array}$	About point	MG road-map	equation
θ				Draw		· ()

Solution and simulation link at <u>www.MotionGenesis.com</u> \Rightarrow <u>Textbooks</u> \Rightarrow <u>Resources</u>.

MG road-map: Inverted pendulum on cart (x and θ) (2D) 20.5.3

A rigid rod B is pinned to a massive cart A (modeled as a particle) that translates horizontally in a Newtonian reference frame N. The cart's position vector from a point $N_{\rm o}$ fixed in N is $x \, \hat{\mathbf{n}}_{\rm x}$ ($\hat{\mathbf{n}}_{\rm x}$ is horizontally-right). B's swinging motion in N is in a vertical plane perpendicular to $\widehat{\mathbf{n}}_{\mathbf{z}}$ (a unit vector fixed in both B and N).

Variable	Translate/ Rotate	Direction (unit vector)	System S	$\begin{array}{c} \text{FBD} \\ \text{of } S \end{array}$	About point	MG road-map equation	Hom
x				Draw	Not applicable	$\bullet \left(\begin{array}{c} = \\ (20.1) \end{array} \right)$	com
θ				Draw			calcı

Note: $m^S * {}^N \vec{\mathbf{a}}^{S_{cm}} = m^A * {}^N \vec{\mathbf{a}}^A + m^B * {}^N \vec{\mathbf{a}}^{B_{cm}}$ and $\frac{{}^N d^N \vec{\mathrm{H}}^{B/A}}{dt} + \dots = {}_{(20.6)} \mathbf{I}_{zz}^{B/A} * {}^N \vec{\mathbf{a}}^B + m^B * \vec{\mathbf{r}}^{B_{cm}/A} \times {}^N \vec{\mathbf{a}}^A.$

ework 15.8 Chapter 24 lete these lations.





 $\stackrel{\circ}{=}_{(15.3)} \mathbf{I}_{zz}^{A/A_{o}}$

 A_{o}



20.5.4 MG road-map: Rotating rigid body (3D)

Shown right is a rotating rigid body B (e.g., tennis racquet, spacecraft, or aircraft) in a Newtonian reference frame N. Right-handed orthogonal unit vectors $\hat{\mathbf{b}}_{\mathbf{x}}$, $\hat{\mathbf{b}}_{\mathbf{y}}$, $\hat{\mathbf{b}}_{\mathbf{z}}$ are fixed in B.



Note: The "about point" is somewhat arbitrary. When $B_{\rm cm}$ is chosen: $\stackrel{N}{\operatorname{H}} \stackrel{\mathcal{H}B_{\rm cm}}{\underset{(15.2)}{\overset{\mathbb{H}}{\operatorname{I}}}} = \stackrel{\mathcal{H}B_{\rm cm}}{\overset{\mathbb{H}}{\operatorname{I}}} \cdot \stackrel{N}{\omega} \stackrel{\mathcal{H}B_{\rm cm}}{\overset{\mathbb{H}B_{\rm cm}}{\operatorname{I}}} \cdot \stackrel{N}{\varepsilon} \stackrel{\mathcal{H}B_{\rm cm}}{\overset{\mathbb{H}B_{\rm cm}}{\operatorname{I}}} \cdot \stackrel{N}{\varepsilon} \stackrel{\mathcal{H}B_{\rm cm}}{\overset{\mathbb{H}B_{\rm cm}}{\operatorname{I}}} \cdot \stackrel{N}{\varepsilon} \stackrel{\mathcal{H}B_{\rm cm}}{\varepsilon} \cdot \stackrel{\mathcal{H}B_{\rm cm}}{\operatorname{I}}$

20.5.5 MG road-map: Bridge crane equations of motion (2D)

A payload (particle) Q is welded to the end of a light rigid cable B which swings in a Newtonian reference frame N. Cable B is pinned to a massive trolley A. Trolley A moves horizontally along a smooth slot fixed in N with a **specified** (known) displacement x(t) due to a force of measure F_x (a linear actuator connects A to a point N_0 of N).



MG road-map for pendulum angle θ , actuator force F_x , and cable tension

Variable	Translate/ Rotate	Direction (unit vector)	$\stackrel{ m System}{S}$	$\begin{array}{c} \text{FBD} \\ \text{of } S \end{array}$	About point	$MG\ road\ map\ equation$
θ				Draw		
F_x				Draw	Not applicable	
Tension				Draw	Not applicable	

Student/Instructor version at <u>www.MotionGenesis.com</u> \Rightarrow <u>Textbooks</u> \Rightarrow <u>Resources</u> Note: Only the θ road-map equation is needed to predict this system's motion. The others are shown for illustrative purposes.

20.5.6 MG road-map: Particle on spinning slot (2D)

A particle Q slides on a straight slot B. The slot is connected with a revolute joint to a Newtonian frame N at point B_0 so that B rotates in a horizontal plane perpendicular to $\hat{\mathbf{b}}_z$ ($\hat{\mathbf{b}}_z$ is vertically-upward and fixed in both B and N). Note: Homework 14.7 completes the MG road-map calculations for x and θ .



MG road-map for x, θ , and F_N ($\hat{\mathbf{b}}_v$ measure of normal force on Q from B)

Variable	Translate/ Rotate	Direction (unit vector)	System	$ \begin{array}{c} \text{FBD} \\ \text{of } S \end{array} $	About point	$MG\ road\mathchar`{map}\ \epsilon$	equation		
x				Draw	Not applicable	• (=)		
θ				Draw	$B_{ m o}$	• ()		
F_N				Draw	Not applicable	• ()		

Note: The F_N road-map equation is needed to predict motion if a friction force depends on μF_N .

$${}^{N}\vec{\mathrm{H}}^{S/B_{\mathrm{o}}} = {}^{N}\vec{\mathrm{H}}^{B/B_{\mathrm{o}}} + {}^{N}\vec{\mathrm{H}}^{Q/B_{\mathrm{o}}} \text{ where } {}^{N}\vec{\mathrm{H}}^{B/B_{\mathrm{o}}} = {}_{(15.3)}I_{zz} {}^{N}\vec{\boldsymbol{\omega}}^{B} \text{ and } {}^{N}\vec{\mathrm{H}}^{Q/B_{\mathrm{o}}} = {}_{(10.3)}\vec{\mathrm{r}}^{Q/B_{\mathrm{o}}} \times m^{Q} {}^{N}\vec{\mathrm{v}}^{Q}.$$

20.5.7 MG road-map: Chaotic motion of a double pendulum (3D)

The schematic to the right shows a swinging babyboot attached by a shoelace to a rigid support. The mechanical model of the babyboot consists of a thin uniform rod A attached to a fixed support N by a revolute joint at point $N_{\rm o}$ and a uniform plate B connected to A with a second revolute joint at point $B_{\rm o}$ so B can rotate freely about A's axis. Note: The revolute joints' axes are *perpendicular*, not parallel.

Modeling considerations

- The plate, rod, and support are rigid.
- The revolute joints are ideal (massless, frictionless, no slop/flexibility).
- Earth is a Newtonian reference frame.
- Forces due to Earth's gravitation are uniform and constant.
- Other distance forces (electromagnetic and gravitational) and air-resistance are negligible.

Right-handed sets of unit vectors $\hat{\mathbf{n}}_x$, $\hat{\mathbf{n}}_y$, $\hat{\mathbf{n}}_z$; $\hat{\mathbf{a}}_x$, $\hat{\mathbf{a}}_y$, $\hat{\mathbf{a}}_z$; $\hat{\mathbf{b}}_x$, $\hat{\mathbf{b}}_y$, $\hat{\mathbf{b}}_z$ are fixed in N, A, B, respectively, with $\hat{\mathbf{n}}_x = \hat{\mathbf{a}}_x$ parallel to the revolute axis joining A to N, $\hat{\mathbf{n}}_z$ vertically-upward, $\hat{\mathbf{a}}_z = \hat{\mathbf{b}}_z$ parallel to the revolute axis joining B to A), and $\hat{\mathbf{b}}_z$ perpendicular to plate B.

Complete the *MG* road-map for angles q_A (angle from $\hat{\mathbf{n}}_z$ to $\hat{\mathbf{a}}_z$ with $\hat{\mathbf{n}}_x$ sense) and q_B (angle from $\hat{\mathbf{a}}_y$ to $\hat{\mathbf{b}}_y$ with $\hat{\mathbf{a}}_z$ sense). Note: The "about point" can be shifted from B_0 to B_{cm} since $\hat{\mathbf{b}}_z \cdot \vec{\mathbf{M}}_{(17.4)}^{B/B_{cm}} = \hat{\mathbf{b}}_z \cdot \vec{\mathbf{M}}_{(17.4)}^{B/B_0}$.

Variable	Translate/ Rotate	Direction (unit vector)	System S	$\begin{array}{c} \text{FBD} \\ \text{of } S \end{array}$	About point	MG road-map equation
q_A				Draw		
q_B				Draw		
	Ctorel and /Terest		4 Ν <i>Π</i> - 4	· · · · · · · · · · · · · · · · · · ·		

Student/Instructor version at <u>www.MotionGenesis.com</u> \Rightarrow <u>Textbooks</u> \Rightarrow <u>Resources</u>

20.5.8 MG road-map: Classic particle pendulum (2D)

A particle Q is welded to the distal end of a light rigid rope B. The rope's other end attaches to a point B_0 , fixed in a Newtonian reference frame N. The swinging motion of B and Q is in a vertical plane that is perpendicular to unit vector $\hat{\mathbf{b}}_z$.

MG road-map for pendulum angle θ and tension F_u ($\hat{\mathbf{b}}_v$ measure of force on Q from B)

Variable	Translate/ Rotate	Direction (unit vector)	System S	$ \begin{array}{c} \text{FBD} \\ \text{of } S \end{array} $	About point	MG road-map	equation	1	mg
θ				Draw		• (=)		
F_y				Draw	Not applicable	• (= (20.1))		

Solution and simulation link at <u>www.MotionGenesis.com</u> \Rightarrow <u>Textbooks</u> \Rightarrow <u>Resources</u>. Draw FBDs Note: Only the θ road-map equation is needed to predict motion. The other is shown for illustrative purposes.



Many additional MG road-map examples at www.MotionGenesis.com \Rightarrow Textbooks \Rightarrow Resources.



20.5.9 MG road-map: Dynamicist on a turntable (ice-skater)

A dynamics instructor stands on a spinning turntable and swings a heavy dumbbell Q inward and outward to change his spin-rate (similar to the ice-skater). Q is modeled as a particle rigidly attached (welded) to the end of the instructor's hands.

The schematic (below-right) shows a rigid body A (modeling the instructor's legs, torso, and head) that rotates (without friction) relative to Earth (a Newtonian reference frame N) about a vertical axis that is fixed in both A and N and which passes through both point $N_{\rm o}$ of N and point $A_{\rm cm}$ (A's center of mass).

A massless rigid arm B (modeling the instructor's arms and hands) attaches to A by a revolute motor (shoulder/muscles) whose revolute axis is horizontal and located at point $B_{\rm o}$ of B ($B_{\rm o}$ lies on the vertical axis connecting $N_{\rm o}$ and $A_{\rm cm}$).

The motor (muscles) **specifies** *B*'s angle $\theta_{\rm B}$ relative to *A* to change in a known (prescribed) manner from 0 to π rad in 4 seconds $(\theta_{\rm B} = \pi \frac{t}{4})$.

Right-handed orthogonal unit vectors $\hat{\mathbf{a}}_x$, $\hat{\mathbf{a}}_y$, $\hat{\mathbf{a}}_z$ and $\hat{\mathbf{b}}_x$, $\hat{\mathbf{b}}_y$, $\hat{\mathbf{b}}_z$ are fixed in A and B, respectively, with $\hat{\mathbf{a}}_y$ vertically-upward, $\hat{\mathbf{b}}_z = \hat{\mathbf{a}}_z$ parallel to the revolute motor's axis, and $\hat{\mathbf{b}}_y$ directed from Q to B_0 .

Quantity	Symbol	Type	Value
Earth's gravitational constant	g	Constant	$9.8 \frac{m}{s^2}$
Distance between Q and B_{o}	L	Constant	0.7 m
Mass of Q	m	Constant	12 kg
A's moment of inertia about line $\overline{A_{\rm cm} B_{\rm o}}$	I_{yy}	Constant	$0.6 \mathrm{kg} \mathrm{m}^2$
Angle from $\widehat{\mathbf{a}}_{y}$ to $\widehat{\mathbf{b}}_{y}$ with $^{+}\widehat{\mathbf{a}}_{z}$ sense	$\theta_{\rm B}$	Specified	$0.25 \pi t$ rad
$\hat{\mathbf{a}}_{\mathbf{y}}$ measure of A's angular velocity in N	ω_A	Variable	





Complete the *MG road-map* for the turntable's "spin-rate" ω_A (Note: The "about point" is not unique)

				-		
Variable	Translate/	Direction	$\operatorname{System}_{S}$	FBD of S	About	MC road-man equation
variable	notate	(unit vector)	5	01.5	point	MG roun-map equation
ω_A				Draw		

 ${\it Student/Instructor \ version \ at \ \underline{www.MotionGenesis.com} \ \Rightarrow \ \underline{Textbooks} \ \Rightarrow \ \underline{Resources}$

20.5.10 MG road-map: Instructor on turntable with spinning wheel (3D)

The pictures to the right shows dynamicist Dr. G standing on a spinning turntable and holding a spinning bicycle wheel.

The mechanical model (below right) has a rigid body A (modeling the turntable, legs, torso, and head) that can freely rotate relative to Earth (Newtonian reference frame N) about a vertical axis that is fixed in both A and N and which passes through the center of the turntable (point $N_{\rm o}$) and $A_{\rm cm}$ (A's center of mass).

A light (massless) rigid frame B (modeling the shoulders, arms, hands, and a portion of the bicycle wheel's axle) is attached to A by a revolute motor at point B_0 of B (B_0 lies on the vertical axis passing through $A_{\rm cm}$). The motor's revolute axis passes through points B_0 and $C_{\rm cm}$, is horizontal, and is parallel to $\hat{\mathbf{b}}_{\mathbf{x}} = \hat{\mathbf{a}}_{\mathbf{x}}$.

A rigid bicycle wheel C is attached to B by a frictionless revolute joint whose axis passes through $C_{\rm cm}$ (C's center of mass) and is parallel to $\hat{\mathbf{b}}_{\rm y}$.

Right-handed orthogonal unit vectors $\hat{\mathbf{a}}_x$, $\hat{\mathbf{a}}_y$, $\hat{\mathbf{a}}_z$ and $\hat{\mathbf{n}}_x$, $\hat{\mathbf{n}}_y$, $\hat{\mathbf{n}}_z$ are fixed in A and N, respectively. Initially $\hat{\mathbf{a}}_i = \hat{\mathbf{n}}_i$ (i = x, y, z), and then rigid body A is subjected to a right-handed rotation characterized by $\theta_A \hat{\mathbf{a}}_z$ where $\hat{\mathbf{a}}_z = \hat{\mathbf{n}}_z$ is directed vertically-upward and $\hat{\mathbf{a}}_x$ points from Dr. G's back to front (parallel to the axis of the revolute motor connecting A and B).

Unit vectors $\hat{\mathbf{b}}_{x}$, $\hat{\mathbf{b}}_{y}$, $\hat{\mathbf{b}}_{z}$ are fixed in *B*. Initially $\hat{\mathbf{b}}_{i} = \hat{\mathbf{a}}_{i}$ (i = x, y, z), then *B* is subjected to a θ_{B} $(\hat{\mathbf{a}}_{x} = \hat{\mathbf{b}}_{x})$ right-handed rotation in *A* where $\hat{\mathbf{b}}_{y}$ is directed along the wheel's axle from Dr. G's right-to-left hand. Dr. G changes θ_{B} in a **specified** sinusoid manner with amplitude 30° and period 4 seconds.

Quantity	Sym	bol and type	Value
Mass of C	m^{C}	Constant	2 kg
Distance between $B_{\rm o}$ and $C_{\rm cm}$	L_x	Constant	$0.5 \mathrm{m}$
A's moment of inertia about $B_{\rm o}$ for $\hat{\mathbf{a}}_{\rm z}$	$\mathbf{I}_{\mathbf{z}\mathbf{z}}^A$	Constant	$0.64~\rm kgm^2$
C's moment of inertia about $C_{\rm cm}$ for $\hat{\mathbf{b}}_{\rm x}$	\mathbf{I}^C	Constant	$0.12~\rm kgm^2$
C's moment of inertia about $C_{\rm cm}$ for $\hat{\mathbf{b}}_{\rm y}$	J^C	Constant	$0.24~\rm kgm^2$
Angle from $\widehat{\mathbf{n}}_{\mathrm{x}}$ to $\widehat{\mathbf{a}}_{\mathrm{x}}$ with $+\widehat{\mathbf{n}}_{\mathrm{z}}$ sense	$\theta_{\rm A}$	Variable	
Angle from $\widehat{\mathbf{a}}_y$ to $\widehat{\mathbf{b}}_y$ with ${}^+\widehat{\mathbf{a}}_x$ sense	$\theta_{\rm B}$	Specified	$\frac{\pi}{6}\sin(\frac{\pi}{2}t)$
$\hat{\mathbf{b}}_{\mathrm{y}}$ measure of C's angular velocity in B	ω_C	Variable	0 2



Purchase turntable/bicycle wheel at Arbor-scientific

Complete the *MG* road-map for θ_A and ω_C (the "about points" are not unique).

Variable	Translate/ Rotate	Direction (unit vector)	System S	$\begin{array}{c} \text{FBD} \\ \text{of } S \end{array}$	About point	MG road-map equation
$ heta_{ m A}$				Draw		
ω_C				Draw		

 ${\it Student/Instructor\ version\ at\ \underline{www.MotionGenesis.com}\ \Rightarrow\ \underline{Textbooks}\ \Rightarrow\ \underline{Resources}}$



20.5.11 MG road-map: Bear riding a unicycle on a high-wire (3D)

The figures to the right show a (massless) pulley-wheel B that <u>rolls</u> along a taut (rigid) cable N (fixed on Earth, a Newtonian frame). Rigid body C (seat, rider, and balancing poles) attach to B with an ideal revolute motor at $B_{\rm o}$ (B's centroid). The motor axis is aligned with B's symmetry axis.

Right-handed orthogonal unit vectors $\hat{\mathbf{n}}_{x}$, $\hat{\mathbf{n}}_{y}$, $\hat{\mathbf{n}}_{z}$ are fixed in N with $\hat{\mathbf{n}}_{z}$ vertically-upward and $\hat{\mathbf{n}}_{x}$ directed horizontally along the cable from a point N_{o} (fixed in N) to B_{N} (B's rolling point of contact with N).

Right-handed orthogonal unit vectors $\hat{\mathbf{a}}_x$, $\hat{\mathbf{a}}_y$, $\hat{\mathbf{a}}_z$ are directed with $\hat{\mathbf{a}}_x = \hat{\mathbf{n}}_x$, $\hat{\mathbf{a}}_y$ parallel to the motor axis, and $\hat{\mathbf{a}}_z$ from B_N to B_0 .

Right-handed unit vectors $\hat{\mathbf{c}}_{x}$, $\hat{\mathbf{c}}_{y}$, $\hat{\mathbf{c}}_{z}$ are parallel to C's principal inertia axes about $C_{\rm cm}$ (C's center of mass), with $\hat{\mathbf{c}}_{y} = \hat{\mathbf{a}}_{y}$ and $\hat{\mathbf{c}}_{z}$ from $B_{\rm o}$ to $C_{\rm cm}$ (with balancing poles, $C_{\rm cm}$ is below $B_{\rm o}$ and L_{C} is negative).

Quantity	Symbol	Type	Value
Earth's gravitational constant	g	Constant	$9.8 \mathrm{m/s^2}$
Radius of B	r_B	Constant	$30~{\rm cm}$
$\hat{\mathbf{c}}_{z}$ measure of C_{cm} 's position vector from B_{o}	L_C	Constant	$-35~\mathrm{cm}$
Mass of C	m^{C}	Constant	2 kg
C's moment of inertia about $C_{\rm cm}$ for $\hat{\mathbf{c}}_{\rm x}$	Ι	Constant	3.4 kg m^2
C's moment of inertia about $C_{\rm cm}$ for $\hat{\mathbf{c}}_{\rm y}$	J	Constant	3.2 kg m^2
C's moment of inertia about $C_{\rm cm}$ for $\hat{\mathbf{c}}_{\rm z}$	K	Constant	2.8 kg m^2
$\hat{\mathbf{a}}_{\mathbf{y}}$ measure of motor torque on <i>B</i> from <i>C</i>	T_y	Specified	below
Angle from $\hat{\mathbf{n}}_z$ to $\hat{\mathbf{a}}_z$ with $-\hat{\mathbf{n}}_x$ sense	q_A	Variable	
$\hat{\mathbf{a}}_{y}$ measure of ${}^{A}\vec{\boldsymbol{\omega}}^{B} ({}^{A}\vec{\boldsymbol{\omega}}^{B} = \omega_{B}\hat{\mathbf{a}}_{y})$	ω_B	Variable	
Angle from $\hat{\mathbf{a}}_z$ to $\hat{\mathbf{c}}_z$ with $+\hat{\mathbf{a}}_y$ sense	q_C	Variable	
$\hat{\mathbf{n}}_{\mathbf{x}}$ measure of $\vec{\mathbf{r}}^{~B_N/N_{\mathrm{o}}}$	x	Variable	



Form a complete set of MG road-maps for this systems's equations of motion (solution is not unique). If necessary, add more MG road-maps so there are the same number of equations as unknowns.

Variable	Translate/ Rotate	Direction (unit vector)	$\mathop{\rm System}_S$	$_{\mathrm{of}\ S}^{\mathrm{FBD}}$	About point	MG road-map equation	Additional Unknowns	
q_A				Draw				
ω_B				Draw				
q_C				Draw				
x				Draw				
* Additional scalar constraint equation(s):								
To move the uniquele to r_{-} , $r_{-} = 10$ m, use a "PD control low" with $T_{-} = -0.3 (r_{-}, r_{-}, r_{-}) = 0.6 \dot{r}$								



20.5.12 MG road-map: Four-bar linkage statics (2D)

The figure to the right shows a planar four-bar linkage consisting of frictionless-pin-connected uniform rigid links A, B, and C and ground N.

- Link A connects to N and B at points A_0 and A_B
- Link B connects to A and C at points B_{o} and B_{C}
- Link C connects to N and B at points $C_{\rm o}$ and C_B
- Point $N_{\rm o}$ of N is coincident with $A_{\rm o}$
- Point N_C of N is coincident with C_o

Right-handed orthogonal unit vectors $\hat{\mathbf{a}}_{i}$, $\hat{\mathbf{b}}_{i}$, $\hat{\mathbf{c}}_{i}$, $\hat{\mathbf{n}}_{i}$ (i = x, y, z) are fixed in A, B, C, N, with:

- $\widehat{\mathbf{a}}_{\mathbf{x}}$ directed from $A_{\mathbf{o}}$ to A_{B}
- $\hat{\mathbf{b}}_{\mathbf{x}}$ directed from $B_{\mathbf{o}}$ to B_C
- $\hat{\mathbf{c}}_{\mathbf{x}}$ directed from $C_{\mathbf{o}}$ to C_B
- $\widehat{\mathbf{n}}_{\mathbf{x}}$ vertically-downward
- $\widehat{\mathbf{n}}_{\mathrm{v}}$ directed from N_{o} to N_{C}
- $\widehat{\mathbf{a}}_z = \widehat{\mathbf{b}}_z = \widehat{\mathbf{c}}_z = \widehat{\mathbf{n}}_z$ parallel to pin axes

As in Hw 8.7, create the following "loop equation" and dot-product with $\hat{\mathbf{n}}_{x}$ and $\hat{\mathbf{n}}_{y}$.

$$L_A \,\widehat{\mathbf{a}}_{\mathrm{x}} + L_B \,\widehat{\mathbf{b}}_{\mathrm{x}} - L_C \,\widehat{\mathbf{c}}_{\mathrm{x}} - L_N \,\widehat{\mathbf{n}}_{\mathrm{y}} = \vec{\mathbf{0}}$$



Quantity	Symbol	Value		
Length of link A	L_A	1 m		
Length of link B	L_B	$2 \mathrm{m}$		
Length of link C	L_C	2 m		
Distance between $N_{\rm o}$ and N_C	L_N	1 m		
Mass of A	m^A	10 kg		
Mass of B	m^B	20 kg		
Mass of C	m^{C}	20 kg		
Earth's gravitational acceleration	g	$9.81 \frac{m}{s^2}$		
$\widehat{\mathbf{n}}_{\mathrm{y}}$ measure of force applied to C_B	H	200 N		
Angle from $\widehat{\mathbf{n}}_x$ to $\widehat{\mathbf{a}}_x$ with ${}^+ \widehat{\mathbf{n}}_z$ sense	q_A	Variable		
Angle from $\widehat{\mathbf{n}}_{\mathrm{x}}$ to $\widehat{\mathbf{b}}_{\mathrm{x}}$ with $^{+}\widehat{\mathbf{n}}_{\mathrm{z}}$ sense	q_B	Variable		
Angle from $\widehat{\mathbf{n}}_{\mathrm{x}}$ to $\widehat{\mathbf{c}}_{\mathrm{x}}$ with $^{+}\widehat{\mathbf{n}}_{\mathrm{z}}$ sense	\bar{q}_C	Variable		

Complete the following *MG* road-map to determine this systems's static configuration.

Variable	Translate/ Rotate	Direction (unit vector)	$\mathop{\rm System}_S$	$_{\mathrm{of}\ S}^{\mathrm{FBD}}$	About point	N	IG road-map equation	n	Additional Unknowns
				Draw					F_x^C, F_y^C
				Draw					F_x^C, F_y^C
				Draw					F_x^C, F_y^C
* Additional scalar constraint equation:			$-L_A \sin(q)$	$-L_A \sin(q_A) \dot{q}_A - L_B \sin(q_B) \dot{q}_B + L_C \sin(q_C) \dot{q}_C = 0$					
* Additional scalar constraint equation:				$L_A \cos(q_A) \dot{q}_A + L_B \cos(q_B) \dot{q}_B - L_C \cos(q_C) \dot{q}_C = 0$					

Determine the *static equilibrium* values of q_A , q_B , q_C . Use your intuition (guess), circle the *stable* solution.

Solution 1	$q_A \approx$	20.0°	$q_B \approx 71.7^{\circ}$	$q_C = 38.3^\circ$
Solution 2	$q_A \approx$	249.3°	$q_B \approx 140.2^\circ$	$q_C = 199.1^{\circ}$
Solution 3	$q_A \approx$	30.7°	$q_B \approx 226.1^\circ$	$q_C = 254.7^{\circ}$

Solution at <u>www.MotionGenesis.com</u> \Rightarrow <u>Get Started</u> \Rightarrow Four-bar linkage



Courtesy Design Simulation Technology